

3<sup>rd</sup> sem. Fluid Mechanics  
sol<sup>n</sup> of mid term question paper.

(i) velocity potential:- It is defined as a scalar function of space and time such that its -ve derivative with respect to any direction gives the velocity of fluid in that direction. It is denoted as ' $\phi$ '

for steady flow,  $\phi = f(x, y, z)$  i.e.  $u = -\frac{\partial \phi}{\partial x}$ ,  $v = -\frac{\partial \phi}{\partial y}$ ,  $w = -\frac{\partial \phi}{\partial z}$

where  $u, v, w$  are the component of velocity in  $x, y$  and  $z$  dir<sup>n</sup> respectively.

\* stream function:- It is defined as scalar function of space & time such that its partial derivative w.r.t. any dir<sup>n</sup> gives the velocity components at right angles to that dir<sup>n</sup>. It is denoted by ' $\psi$ '

i.e.  $\frac{\partial \psi}{\partial x} = v$ , and  $\frac{\partial \psi}{\partial y} = -u$

Here,  $u, v$  are the component of velocity in  $x$  and  $y$  dir<sup>n</sup> respectively.

Q.2:- Statement:- "In a steady flow, the sum of all forms of energy in a fluid along a streamline is the same at all points on that streamline."

Assumption:- The following assumptions to be made in derivation of Bernoulli's eq<sup>n</sup>:-

- (i) The fluid is ideal i.e.  $\mu = 0$ , (ii) The flow is steady
- (iii) The flow is incompressible (iv) The flow is irrotational.

Derivation:- Consider a stream-line in which flow is taking place in  $s$ -dir<sup>n</sup> as shown in fig. Consider a cylindrical element of cross-section ' $dA$ ' and length ' $ds$ '

The resultant force on the fluid element in  $s$ -dir<sup>n</sup>  
 $PdA - (P + \frac{\partial P}{\partial s} ds)dA - \rho g dA \cdot ds \cdot \cos \theta = \rho dA ds \cdot a_s$

$$a_s = \frac{dv}{dt} = \frac{\partial u}{\partial s} \cdot \frac{ds}{dt} + \frac{\partial u}{\partial t} = u \frac{\partial u}{\partial s} + \frac{\partial u}{\partial t}$$

For steady flow,  $\frac{\partial u}{\partial t} = 0$

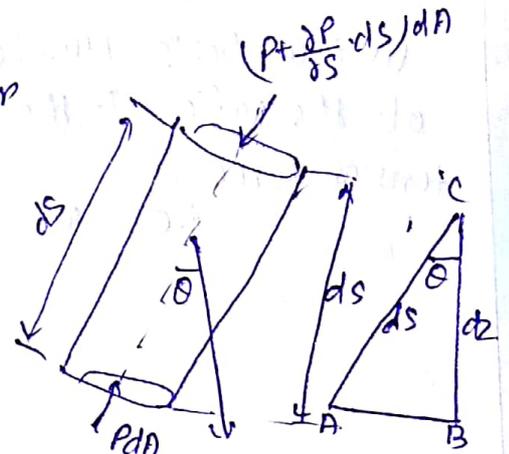
$$a_s = u \frac{\partial u}{\partial s}$$

$$\text{or, } PdA - PdA - \frac{\partial P}{\partial s} \cdot ds \cdot dA - \rho g dA dz = \rho dA ds \cdot u \frac{\partial u}{\partial s}$$

$$\Rightarrow -dA \cdot ds \left( \frac{\partial P}{\partial s} + \rho g \frac{dz}{ds} + \rho u \frac{\partial u}{\partial s} \right) = 0$$

$$\text{or, } \frac{\partial P}{\partial s} + \rho g \frac{dz}{ds} + \rho u \frac{\partial u}{\partial s} = 0$$

$$\Rightarrow \boxed{\frac{dP}{\rho} + u du + g dz = 0}$$



$$W = mg = \rho \cdot dA \cdot ds \cdot g$$

In  $\Delta ABC$

$$\cos \theta = \frac{dz}{ds}$$

$$ds \cos \theta = dz$$

gkm

Now integrating the eqn.

$$\int \frac{\partial P}{\rho} + \int g dz + \int u du = \text{const.}$$

If flow is incompressible. i.e.  $\rho$  is const.

$$\frac{P}{\rho} + gz + \frac{u^2}{2} = \text{const.}$$

$$\text{i.e. } \frac{P_1}{\rho g} + \frac{u_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{u_2^2}{2g} + z_2$$

where  $\frac{P_1}{\rho g} =$  Pressure head,  $\frac{u^2}{2g} =$  Kinetic head, and  $z =$  Potential head

Q.3. Reynold's no.:- It is defined as the ratio of Inertia force of a flowing fluid and the viscous force of the fluid.

$$\text{i.e. } Re = \frac{\text{Inertia force } (F_i)}{\text{viscous force } (F_v)} = \frac{\rho v L}{\mu} = \frac{v L}{\nu}$$

(ii) Froude's Number ( $F_e$ ).:- It is defined as the square root of the ratio of inertia force of a flowing fluid to the gravity force.

$$\text{i.e. } F_e = \sqrt{\frac{\text{inertia force } (F_i)}{\text{gravity force } (F_g)}} = \frac{v}{\sqrt{Lg}}$$

(iii) Mach's Number ( $M$ ) :- It is defined as the square root of the ratio of the inertia force of a fluid to the elastic force.

$$\text{i.e. } M = \sqrt{\frac{\text{Inertia force}}{\text{Elastic force}}} = \sqrt{\frac{F_i}{F_e}} = \frac{v}{\sqrt{K/\rho}} = \frac{v}{c}$$

(iv) Weber's Number ( $We$ ) = It is defined as the square root of the ratio of the inertia force of a flowing fluid to the surface tension force.

$$\text{i.e. } We = \sqrt{\frac{F_i}{F_s}} = \frac{v}{\sqrt{\sigma/\rho L}}$$

PK

Q.4. Given

$H = 900\text{mm} = 0.9\text{m}$   
 $Q = 300\text{lit/sec} = 0.3\text{m}^3/\text{s}$   
 $C_d = 0.62$

we know that

$Q = \frac{2}{3} C_d \times L \times \sqrt{2g} \times H^{3/2}$   
 $0.3 = \frac{2}{3} \times 0.62 \times L \times \sqrt{2 \times 9.81} \times (0.9)^{3/2}$   
 $\therefore L = 0.192\text{m} = 192\text{mm}$

Q.5. Given

$y = 2y - y^2$

$\frac{dy}{dy} = 2 - 2y$

$\mu = 0.4\text{ Poise} = 0.04\text{ N}\cdot\text{s}/\text{m}^2$

(i)  $\left(\frac{dy}{dy}\right)_{y=0} = 2$

$\tau = \mu \cdot \frac{dy}{dy} = 0.04 \left(\frac{dy}{dy}\right)_{y=0} = 0.04 \times 2 = 0.08\text{ N}/\text{m}^2$

(ii)  $\left(\frac{dy}{dy}\right)_{y=0.05} = 2 - 2 \times (0.05) = 2 - 0.1 = 1.9$

$\tau = \mu \cdot \frac{dy}{dy} = 0.04 \left(\frac{dy}{dy}\right)_{0.05} = 0.04 \times 1.9 = 0.076\text{ N}/\text{m}^2$

Q.6. Given

$d_1 = 100\text{mm} = 10\text{cm}$

$a_1 = \frac{\pi}{4} (d_1)^2 = 78.539\text{ cm}^2$

Contraction ratio ( $C_c$ ) = 0.5

Dia. of throat ( $d_2$ ) =  $0.5 \times d_1 = 0.5 \times 10 = 5\text{cm}$

$a_2 = \frac{\pi}{4} (5)^2 = 19.635\text{ cm}^2$

Head of water (for no blow) =  $\frac{P_1}{\rho g} = 3\text{m}$  (gauge)

absolute pressure head =  $3 + 10.3 = 13.3\text{m}$

Total pressure head =  $\frac{P_2}{\rho g} = 2\text{m}$  of water (absolute)

*gan*

$$\text{Diff. in pressure head (absolute)} = \frac{P_1}{\rho g} - \frac{P_2}{\rho g}$$

$$= 13.3 - 2$$

$$= 11.3 = 1130 \text{ cm of water}$$

rate of flow

$$Q_1 = C_d \frac{Q_1 Q_2}{\sqrt{Q_1^2 - Q_2^2}} \quad Q_1 = C_d \frac{Q_1 Q_2}{\sqrt{Q_1^2 - Q_2^2}} \sqrt{2gh}$$

$$= 0.97 \times \frac{78.539 \times 19.635}{\sqrt{(78.539)^2 - (19.635)^2}} \sqrt{2 \times 9.81 \times 1130}$$

$$= 29289.1 \text{ cm}^3/\text{sec}$$

$$= 29.2891 \text{ lit}/\text{sec}$$